

## TUNABLE IMPEDANCE MATCHING CIRCUIT FOR RF POWER AMPLIFIER

### BACKGROUND OF THE INVENTION

The invention relates generally to radio frequency (RF) power amplifiers and, more particularly, to tunable impedance matching circuits for RF power amplifier circuits.

The use of RF power transistor devices as signal amplifiers in wireless communication applications is well known. With the considerable recent growth in the demand for wireless services, such as personal communication services, the operating frequency of wireless networks has increased dramatically and is now well into the gigahertz frequencies. Radio frequency (RF) power transistors are commonly used in amplification stages for radio base station amplifiers. Such transistors are also widely used in other RF-related applications, such as cellular telephones, paging systems, navigation systems, television, avionics, and military applications.

Production of RF power transistor amplifiers on a large-volume basis is traditionally a problem, because of variables that the individual elements possess. In particular, the transistor devices have natural variances in input capacitance, gain and phase shift. Thus, in commercial implementations, significant time and effort is needed to first characterize a particular transistor device over the range of expected operating frequencies and voltages, and then attempt to build many devices using like materials, which deliver similar desired performance. However, due to the variations in transistors' and various other elements over identical operating frequencies and voltages, the ability to successfully tune transistor devices is limited.

Consistent performance of high frequency RF power transistors is, thus, problematic

due to their intrinsic variations. These variances must be compensated for in the amplification circuits to achieve reliable and consistent performance. For example, DC biasing and temperature compensation circuits are traditionally employed in the circuits to compensate for inherent differences between individual power transistor devices and for changes in temperature during operation.

Further, RF power amplifiers must be tuned for optimal performance. Presently, RF power amplifiers are assembled by first placing the circuit's components on a substrate (e.g., a PC board) and securing the RF power transistors in place. The amplifier is then manually or automatically tuned, either of which requires complicated test equipment. Existing manual tuning methods involve adjusting variable capacitors, which are included in the circuits solely for tuning. The capacitors are relatively expensive; thus, their elimination would significantly reduce the cost of a RF power amplifier. Further, the amount of adjustment needed is not easily determined, and the methods used are iterative and sometimes intuitive; thus, the process can be time consuming. Existing automated tuning of RF power amplifiers is complicated, requiring both complicated test equipment and complicated algorithms.

## SUMMARY OF THE INVENTION

In accordance with a first aspect of the invention, a tunable impedance matching circuit is provided for tuning an active device, such as, e.g., a field effect transistor, in a RF power amplifier. The matching circuit includes an adjustable length transmission line for electrically coupling a RF signal between an active device and its source and a load. The length of the transmission line is adjusted to achieve selected performance characteristic(s) of the amplifier, such as, e.g., input return loss, output return loss or gain.

In accordance with another aspect of the invention, a method is provided for tuning an active device, e.g., a RF power transistor, used in an amplifier circuit. The method employs tuning an impedance matching circuit coupled to the active device, the matching circuit including a transmission line having an adjustable length. In an exemplary embodiment, the method includes measuring a performance characteristic of the device, such as, e.g., input return loss, and then adjusting the length of the transmission line to adjust the performance characteristic to a desired level.

In accordance with still another aspect of the invention, a method of manufacturing a power amplifier is provided. The method includes coupling an active device to a matching circuit comprising an adjustable length transmission line. A performance characteristic of the device is then measured, and the length of the transmission line is adjusted to achieve a desired change in the measured performance characteristic.

In embodiments of the forgoing, the transmission line initially has a length slightly greater than a quarter of a wavelength (" $\frac{1}{4} \lambda$ ") of a fundamental frequency of a RF signal being amplified, with the final (i.e., adjusted) length depending on whether the circuit is capacitively or inductively loaded. By way of example, the length of the transmission line

may be adjusted using laser trimming.

Other aspects and features of the present invention will become apparent from the following description taken in conjunction with the accompanying drawings.

1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040	2041	2042	2043	2044	2045	2046	2047	2048	2049	2050	2051	2052	2053	2054	2055	2056	2057	2058	2059	2060	2061	2062	2063	2064	2065	2066	2067	2068	2069	2070	2071	2072	2073	2074	2075	2076	2077	2078	2079	2080	2081	2082	2083	2084	2085	2086	2087	2088	2089	2090	2091	2092	2093	2094	2095	2096	2097	2098	2099	2100	2101	2102	2103	2104	2105	2106	2107	2108	2109	2110	2111	2112	2113	2114	2115	2116	2117	2118	2119	2120	2121	2122	2123	2124	2125	2126	2127	2128	2129	2130	2131	2132	2133	2134	2135	2136	2137	2138	2139	2140	2141	2142	2143	2144	2145	2146	2147	2148	2149	2150	2151	2152	2153	2154	2155	2156	2157	2158	2159	2160	2161	2162	2163	2164	2165	2166	2167	2168	2169	2170	2171	2172	2173	2174	2175	2176	2177	2178	2179	2180	2181	2182	2183	2184	2185	2186	2187	2188	2189	2190	2191	2192	2193	2194	2195	2196	2197	2198	2199	2200	2201	2202	2203	2204	2205	2206	2207	2208	2209	2210	2211	2212	2213	2214	2215	2216	2217	2218	2219	2220	2221	2222	2223	2224	2225	2226	2227	2228	2229	2230	2231	2232	2233	2234	2235	2236	2237	2238	2239	2240	2241	2242	2243	2244	2245	2246	2247	2248	2249	2250	2251	2252	2253	2254	2255	2256	2257	2258	2259	2260	2261	2262	2263	2264	2265	2266	2267	2268	2269	2270	2271	2272	2273	2274	2275	2276	2277	2278	2279	2280	2281	2282	2283	2284	2285	2286	2287	2288	2289	2290	2291	2292	2293	2294	2295	2296	2297	2298	2299	2300	2301	2302	2303	2304	2305	2306	2307	2308	2309	2310	2311	2312	2313	2314	2315	2316	2317	2318	2319	2320	2321	2322	2323	2324	2325	2326	2327	2328	2329	2330	2331	2332	2333	2334	2335	2336	2337	2338	2339	2340	2341	2342	2343	2344	2345	2346	2347	2348	2349	2350	2351	2352	2353	2354	2355	2356	2357	2358	2359	2360	2361	2362	2363	2364	2365	2366	2367	2368	2369	2370	2371	2372	2373	2374	2375	2376	2377	2378	2379	2380	2381	2382	2383	2384	2385	2386	2387	2388	2389	2390	2391	2392	2393	2394	2395	2396	2397	2398	2399	2400	2401	2402	2403	2404	2405	2406	2407	2408	2409	2410	2411	2412	2413	2414	2415	2416	2417	2418	2419	2420	2421	2422	2423	2424	2425	2426	2427	2428	2429	2430	2431	2432	2433	2434	2435	2436	2437	2438	2439	2440	2441	2442	2443
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## BRIEF DESCRIPTION OF THE DRAWINGS

Preferred embodiments of the invention are illustrated by way of example, and not by way of limitation, in the figures of the accompanying drawings, in which like reference numerals refer to like components, and in which:

5           FIG. 1 is a schematic circuit diagram of an inductively coupled, tunable impedance matching circuit for a RF power amplifier circuit, according to one embodiment of the invention;

10           FIG. 2 is a schematic circuit diagram of a capacitively coupled, tunable impedance matching circuit for a RF power amplifier circuit, according to another embodiment of the invention;

15           FIG. 3 is a graph of the frequency response of a RF power amplifier circuit as a function of a length of a transmission line length of an impedance matching circuit, according to one aspect of the invention;

20           FIG. 4 is a schematic circuit diagram of a RF power amplifier circuit employing both input and output tunable impedance matching circuits, according to an embodiment of the invention; and

25           FIG. 5 is a Smith admittance chart illustrating how the frequency of a RF power amplifier circuit can be varied at substantially constant conductance, in accordance with one embodiment of the invention.

## DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

The present invention is directed to the tuning of RF power amplifiers for impedance matching. In particular, the invention involves tuning a performance characteristic of a power amplifier by employing an impedance matching circuit at the input, output, or both, of the active transistor element. In particular, embodiments of the tunable impedance matching circuit include both inductive and capacitively coupled matching structures incorporating a variable length transmission line.

More particularly, the transmission line preferably has an initial length slightly greater than  $\frac{1}{4} \lambda$  of a fundamental frequency of a RF signal being amplified. In order to tune the performance characteristic of the power amplifier, the length of the transmission line is adjusted, such that only the resonance of the impedance matching circuit, and not the resistance, is changed. The resulting length of the transmission line may be slightly greater, slightly less, or approximately the same as  $\frac{1}{4} \lambda$  of the fundamental RF signal frequency, depending on whether the amplifier is capacitively loaded, inductively loaded, or has no reactance component, respectively. Thus, the invention may be applied in matching circuits employed in RF power amplifiers having reactive inputs.

FIG. 1 is a schematic drawing of an inductively coupled, tunable impedance matching circuit ("tuning circuit") 10 for use in a RF power amplifier circuit. The matching circuit 10 is adapted to be attached to a source 12 and a load 14, and may be employed as either an input matching element, or an output matching element, as is described in greater detail in conjunction with FIG. 4. In one embodiment, the matching circuit 10 comprises a circuit of passive components, which are selected depending on the particular application and device requirements.

In accordance with a general aspect of the invention, the tuning circuit 10 further comprises a variable length transmission line 16 for coupling the source 12 to the load 14. As part of the process for assembling a RF power amplifier circuit including the matching circuit 10, the length of the transmission line 16 is adjusted in order to tune a performance characteristic of the amplifier circuit. This may be accomplished, e.g., by laser trimming the physical length of the transmission line 16.

Notably, the resistance of the transformation of the transmission line 16 depends on its width, whereas the frequency of the transformation depends on its length. Therefore, by adjusting only the length of the transmission line 16, the resonance frequency of the matching circuit 10 can be changed, while the resistance at resonance is changed only slightly. More particularly, by definition, a  $\frac{1}{4} \lambda$  transmission line is 90 degrees at resonance.

The impedance ( $Z_0$ ) of that transmission is determined by the desired transformation according to the geometric mean of the generator and load. As an example, to transform 5 ohms to 50 ohms, the width of a  $\frac{1}{4} \lambda$  transmission line is the geometric mean of the two impedances, or  $(5 * 50)^{0.5}$  ohms.

By way of example, the Smith admittance chart in FIG. 5 illustrates how the frequency 48 of a RF power amplifier circuit can be varied from 1.86 GHz (at point 50), to 1.96 GHz (at point 52), to 2.06 GHz (at point 54), at substantially constant 20 mmho conductance, or 50 ohms of resistance (line 56). Lines 58, 60 and 62 illustrate operating points of inductance (line 58), zero susceptance (line 60) and capacitance (line 62), respectively. Notably, it may be observed from the chart in FIG. 5 that as the frequency changes, the conductance remains constant for a significant range of frequencies.

FIG. 2 is a schematic drawing of a capacitively coupled, tunable impedance matching circuit 18. As with the matching circuit 10 of FIG. 1, the matching circuit 18 also includes a variable length transmission line 16 for coupling a source 12 to a load 14. As with matching circuit 10, as part of the process for assembling a RF power amplifier circuit incorporating the matching circuit 18 as either an input or an output matching circuit, the tuning circuit 10 is tuned by adjusting the length of the transmission line 16.

FIG. 3 shows the frequency response characteristics of an exemplary RF power amplifier circuit employing a matching circuit (tuning circuit) having a variable length transmission line 16 of circuits 10 and 18. Line 20 is a graph of the input return loss of the amplifier circuit, and line 24 is a graph of the gain/loss of the two-port circuit. During assembly of the amplifier circuit, e.g., when the amplifier circuit is initially laid out, one or more selected performance characteristics of the amplifier are measured using standard test equipment. For given application(s) of the amplifier, certain performance characteristics will be desired. Such measurable performance characteristics include input return loss, (e.g., as shown by line 20 in FIG. 3). Other measurable performance characteristics include, without limitation, gain and output return loss. As will be appreciated by those skilled in the art, numerous other performance characteristics may be selected without varying from the inventive concepts presented herein.

As noted above, due to the variability of the device characteristics, the desired performance characteristic(s) of the amplifier circuit are not necessarily achieved when the device is first laid out; hence, the need arises to tune the amplifier circuit to achieve the desired characteristics. For example, area 28 shows the frequency range where it might be desired to have the optimum input return loss of the amplifier circuit. In other words, it



would be desirable to shift line 20 to the right until its minimum falls within area 28. By changing the length of the matching circuit transmission line according to known relationship, the input return loss can be predictably shifted, as shown in line 22.

FIG. 4 is a schematic drawing illustrating the use of adjustable matching circuits 36 and 40, e.g., such as either of circuits 10 and 18 in FIGS. 1 and 2, in an exemplary RF power amplifier circuit 30. The amplifier circuit 30 includes an active RF device 32, e.g., a field effect transistor. The transistor 32 receives an input signal at its gate terminal from a source 34, which is coupled to the gate terminal via input matching circuit 36. An amplified output signal is transmitted from a drain terminal of the transistor 32 to a load 38, which is coupled to the drain via output matching circuit 40. The matching circuits 36 and 40 each include a variable length transmission line, as in matching circuits 10 and 18 of FIGS. 1 and 2.

In accordance with this aspect of the invention, the values of the components in each of the matching circuits 36 and 40 are initially determined according to the respective source and load impedance required by the transistor device 32. After assembling the amplifier circuit 30, at least in part, each matching circuit 36 and 40 is tuned to achieve desired electrical performance by changing the length of the respective transmission lines therein.

While preferred embodiments and applications have been shown and described, as can be appreciated by those of ordinary skill in the art, the invention can be embodied in other specific forms without departing from the inventive concepts contained herein. The presently disclosed embodiments, therefore, should be considered as illustrative, and not restrictive.